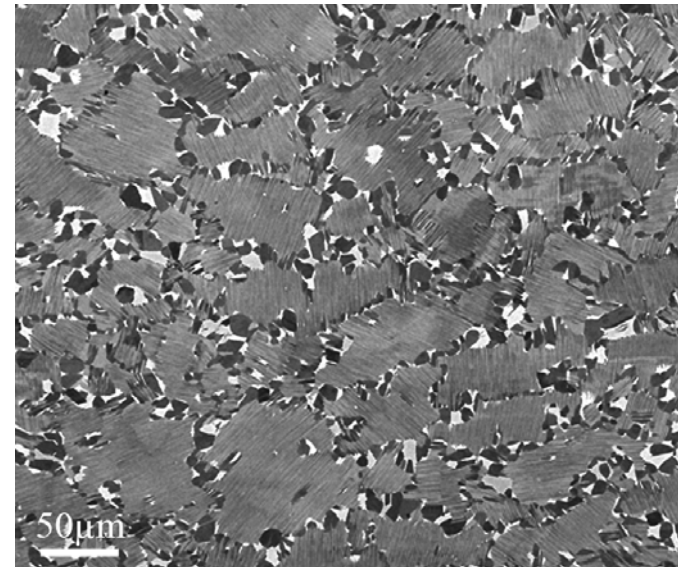
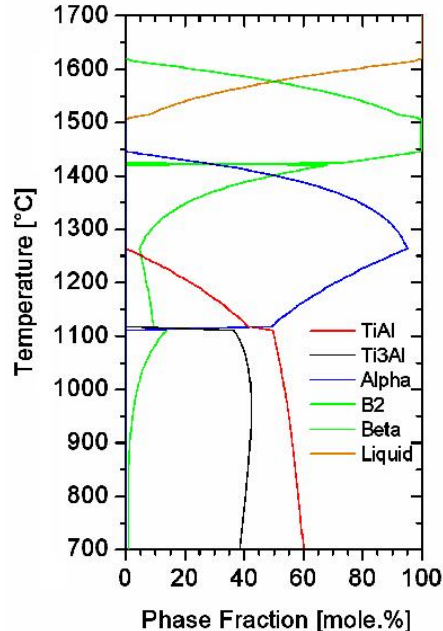




Advanced Intermetallic Titanium Aluminides - Development Status and Perspectives

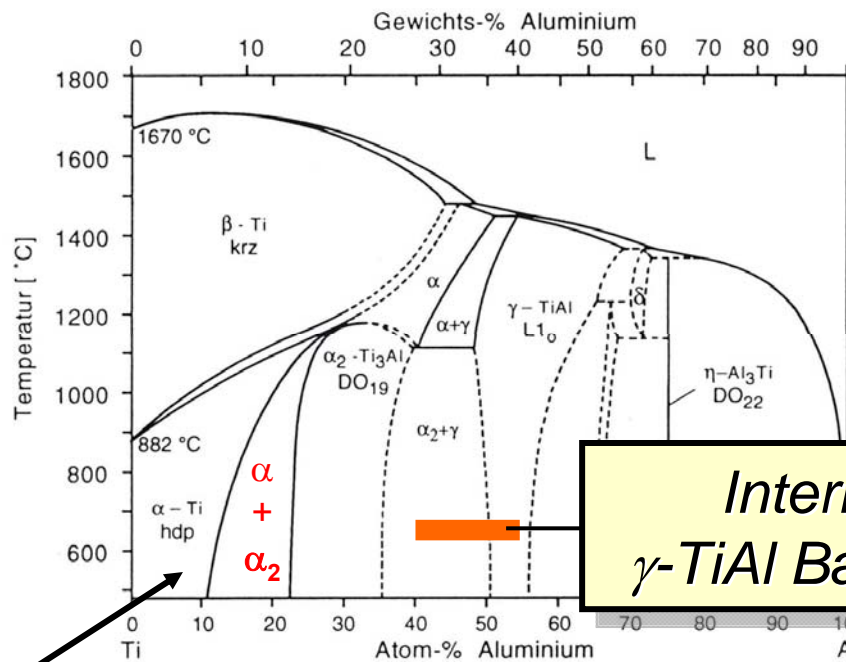
Helmut Clemens and Svea Mayer

Department of Physical Metallurgy and Materials Testing
Montanuniversität Leoben, Austria





Characteristics of Intermetallic Materials & γ -Titanium Aluminides



Intermetallic
 γ -TiAl Based Alloys

$$Al_{equiv.} = Al + 1/3 \cdot Sn + 1/6 \cdot Zr + 10 \cdot (O + C + 2N) < 9 \text{ m-\%}$$

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Titanium and Titanium Alloys

Fundamentals and Applications

DGM



Ordered crystal structures due to strong bonding forces between the metal atoms



Unique mechanical properties

- high Young's moduli, high-temperature strength retention, (low density → **TiAl**)

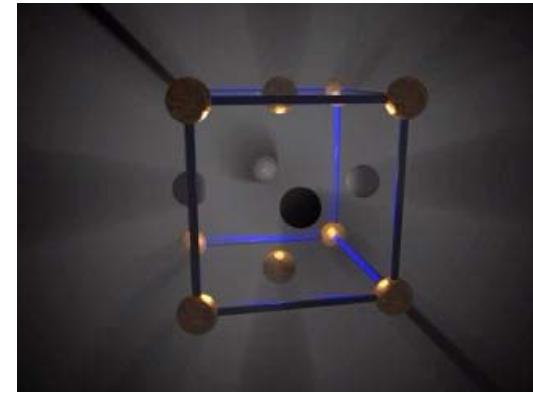
High thermal conductivities

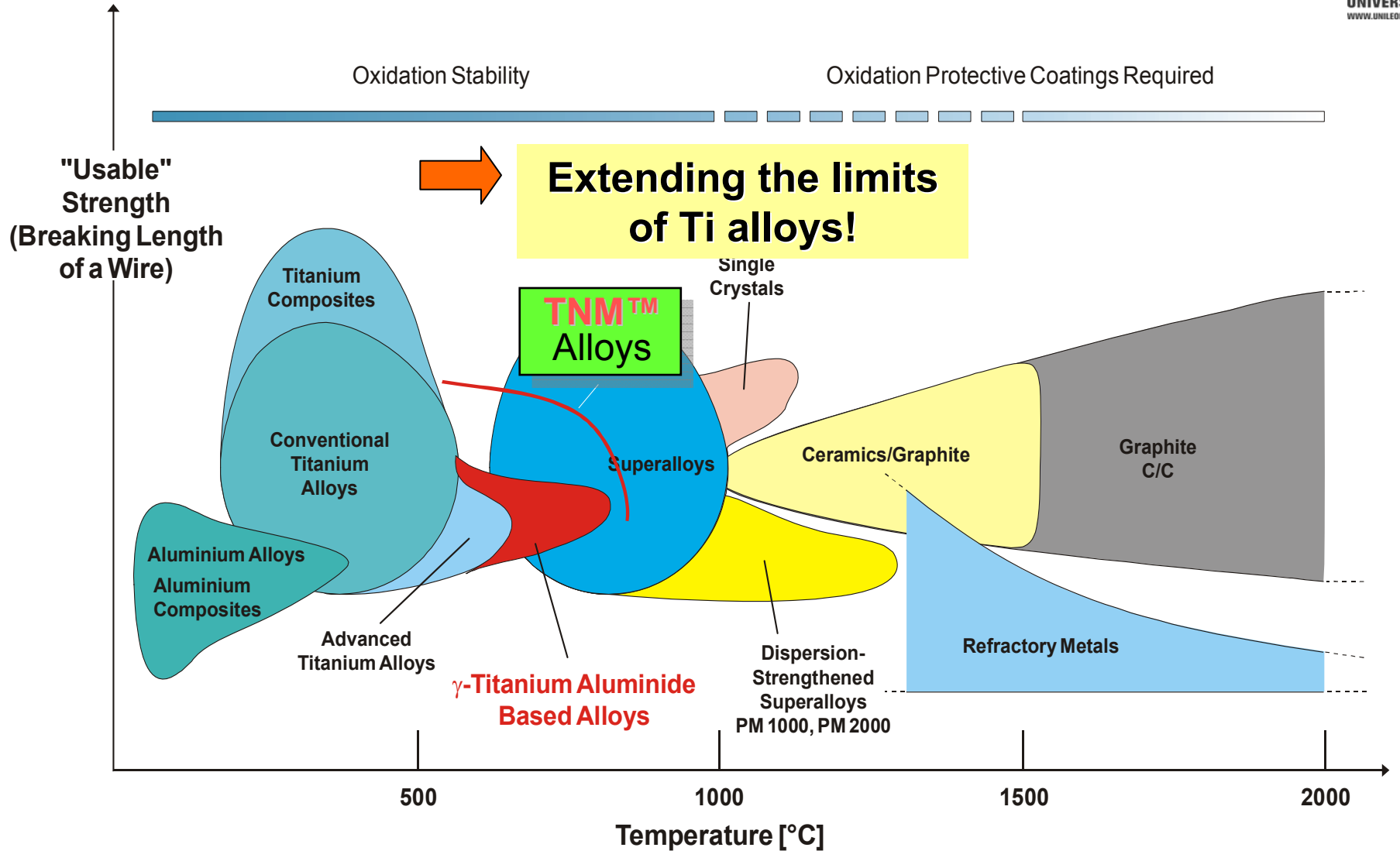
- higher than engineering ceramics ⇒ higher cooling efficiency and lower thermal stresses

“**Ceramic**” behaviour at room temperature -

“**metallic**” behaviour at elevated temperature

- low (**TiAl**) or no (NiAl) ductility at room temperature
- some intermetallics (**TiAl**) can be processed using conventional metallurgical methods ⇒ economically competitive





→ **TNM™ alloys: Ti-(42-45)Al-(3-5)Nb-(0.1-2)Mo-(0.1-1)B**



⇒ **Light weight structural materials:** ~ 4 g/cm³
(50 % less dense than superalloys and steels)

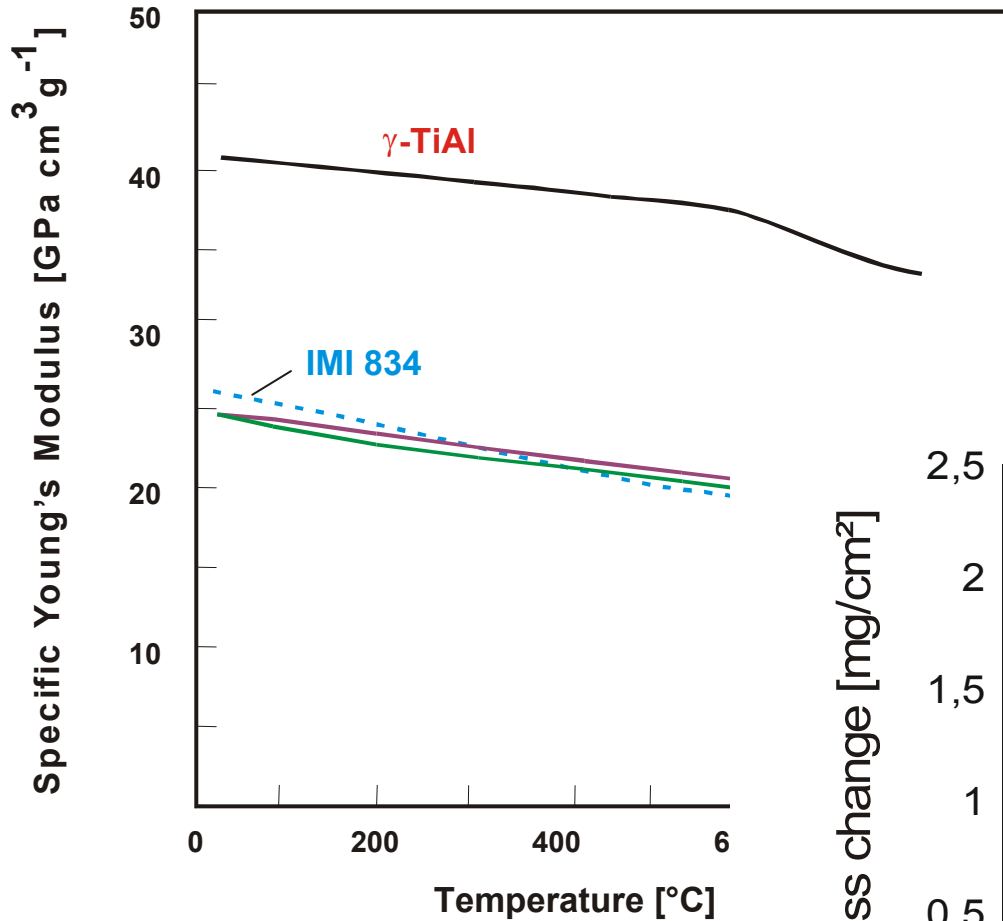
⇒ ...and several other attractive properties

- high specific modulus
- high specific strength
- good oxidation resistance
- resistance against “titanium fire”

To be used in **high-temperature technologies**

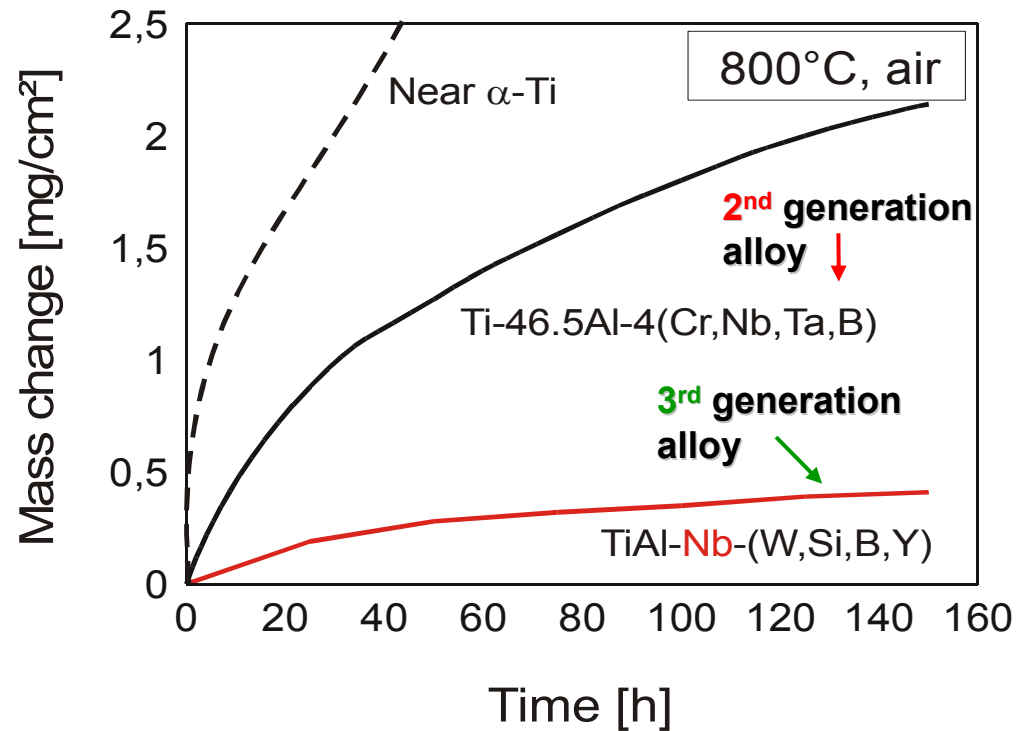
➔ **Aircraft engines, automotive engines**

➔ **Application benefit:** higher efficiency, lower fuel consumption and reduced emissions



Oxidation behavior

Elastic modulus





Physical Metallurgy

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Titanium and Titanium Alloys

Fundamentals and Applications



DGM

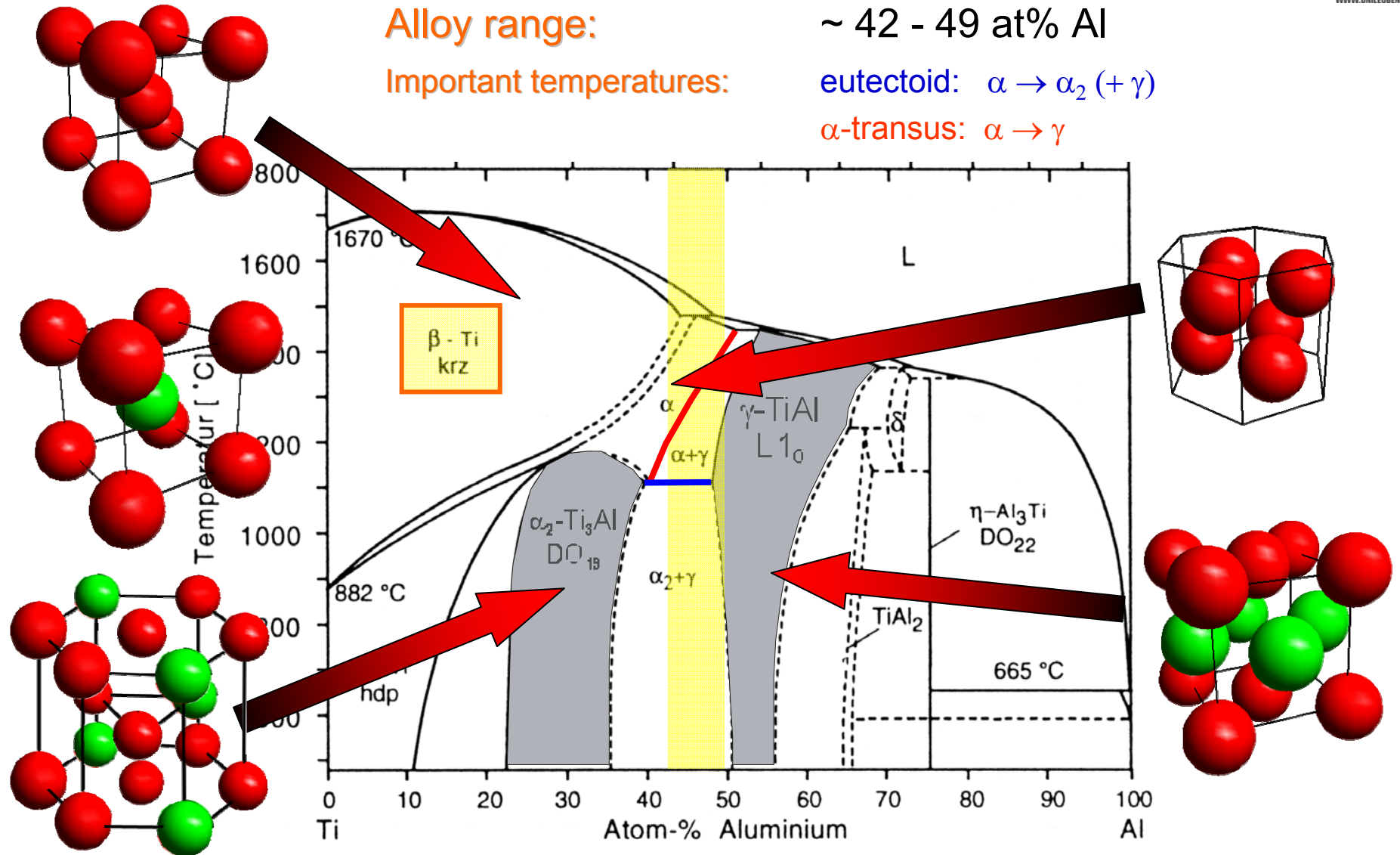
Alloy range:

~ 42 - 49 at% Al

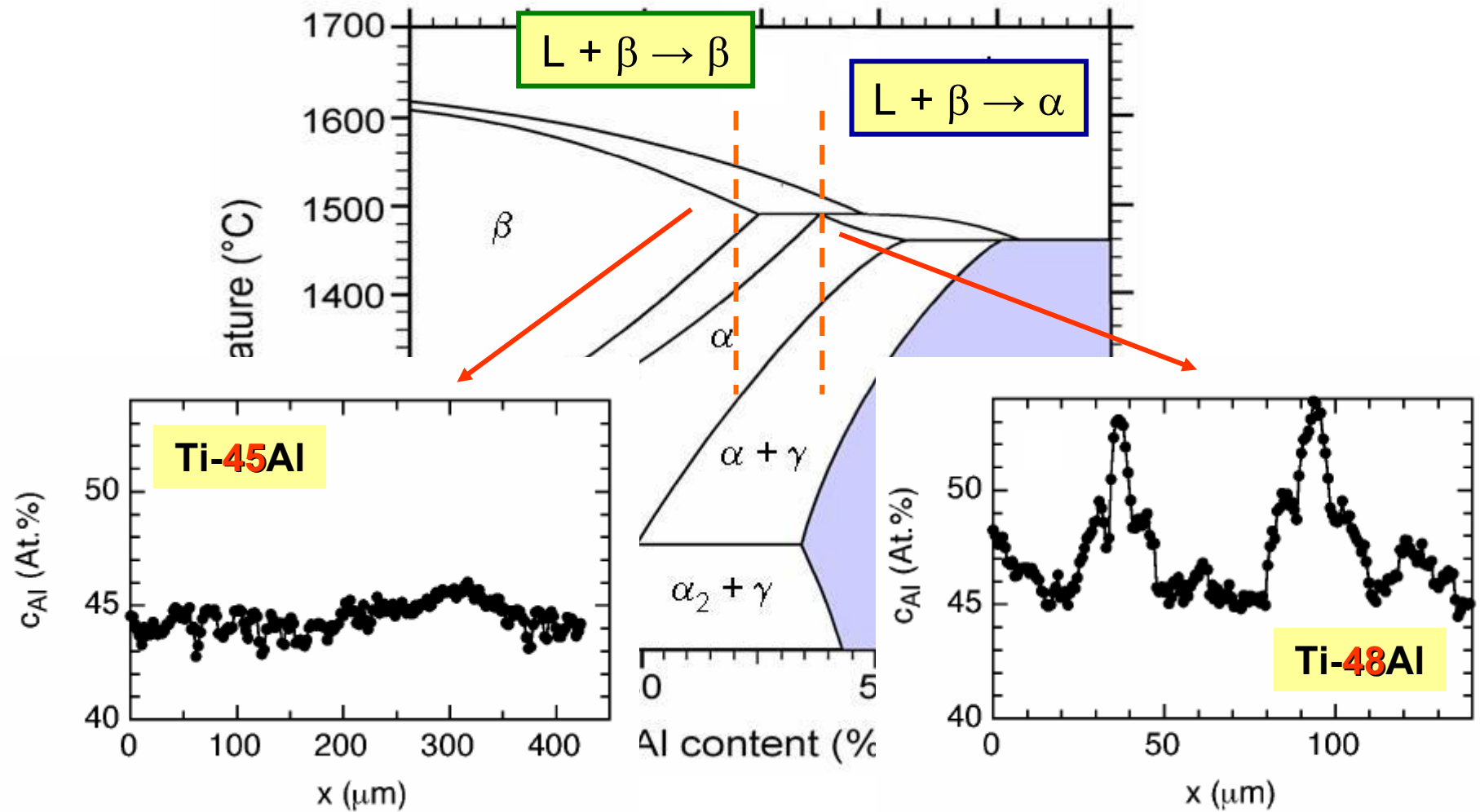
Important temperatures:

eutectoid: $\alpha \rightarrow \alpha_2 (+ \gamma)$

α -transus: $\alpha \rightarrow \gamma$



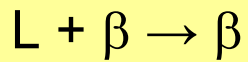
Further phases: borides, silicides, perovskites, Laves-phases, ω -phases, ...



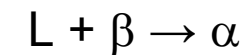
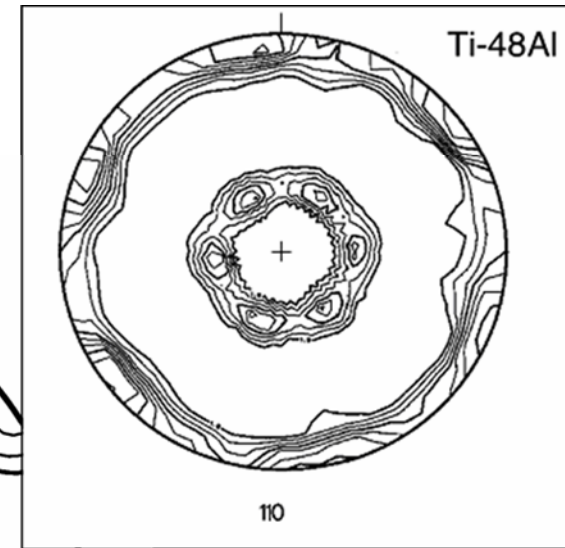
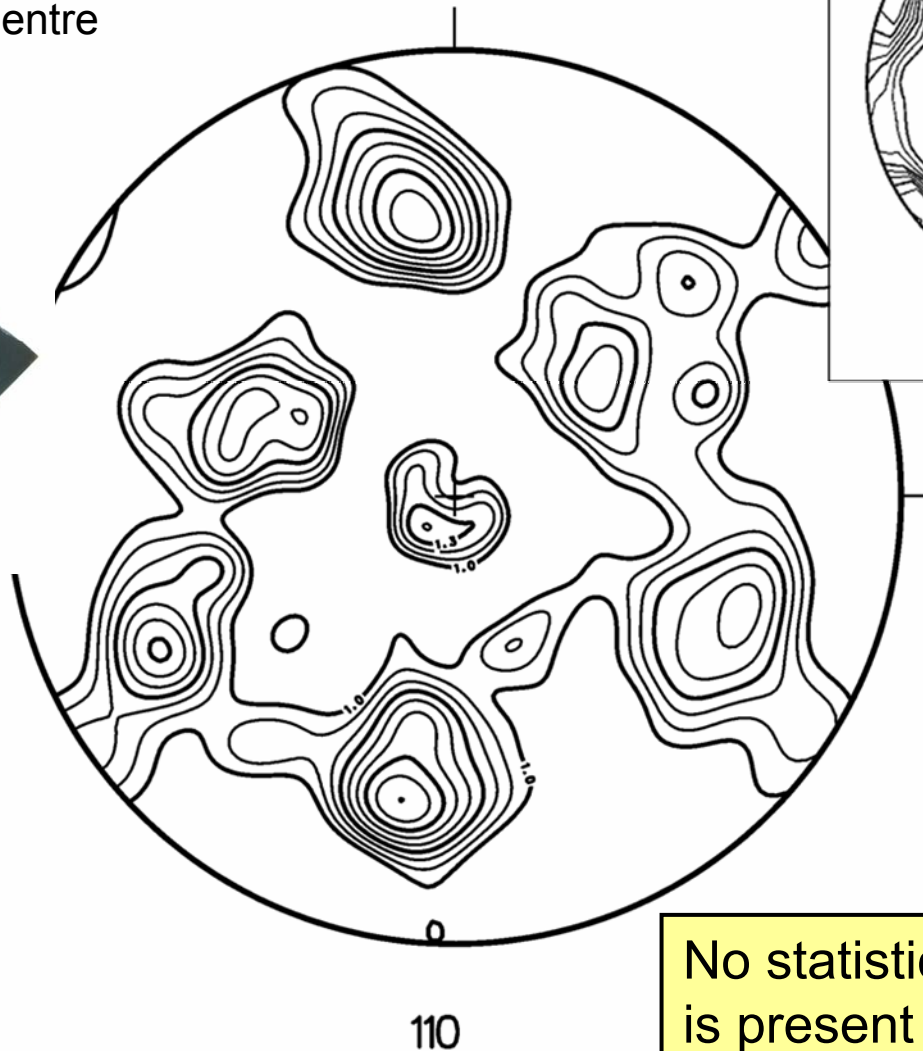
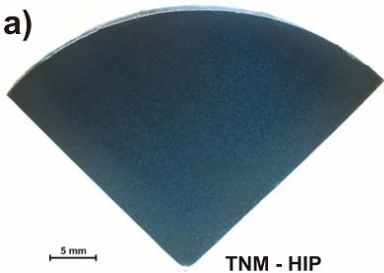
M. Oehring, V. Küstner, A. Chatterjee, V. Güther, H. Clemens, and F. Appel,
Proceedings "Gamma Titanium Aluminides 2003", pp. 89-96.

Neutron diffraction

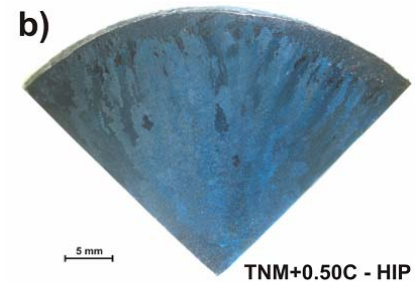
TEX-2 diffractometer,
HZG Research Centre



a)



b)



No statistically significant texture
is present after solidification



α_2 - Ti_3Al
phase

β/β_0 phase

silicides

carbides

Ti - (42-48)Al

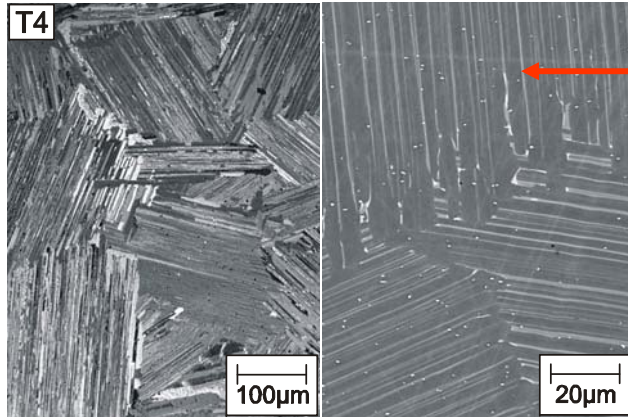
α_2 volume fraction \uparrow
strength \uparrow
RT ductility \downarrow
oxidation resistance \downarrow

refinement of microstructure \uparrow
hot-workability \uparrow
oxidation resistance \uparrow
creep strength \uparrow

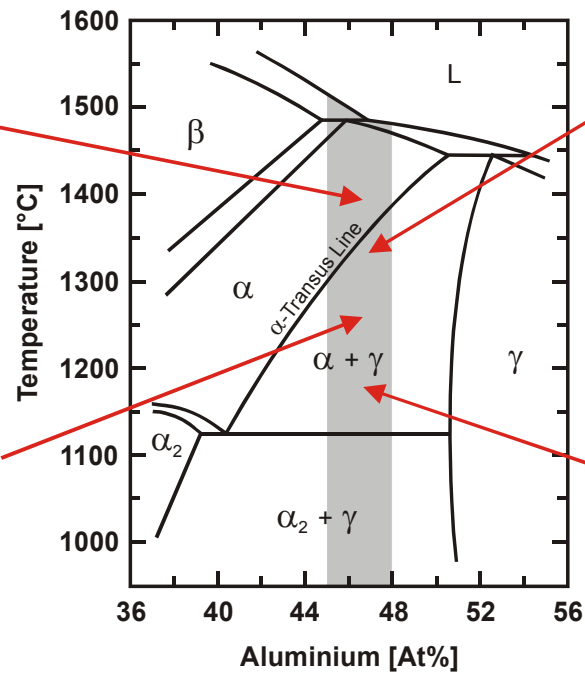
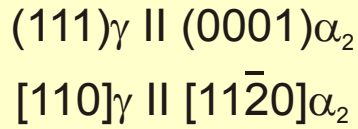
refinement of microstructure \uparrow
creep strength \uparrow

RT ductility \uparrow
superplasticity \uparrow

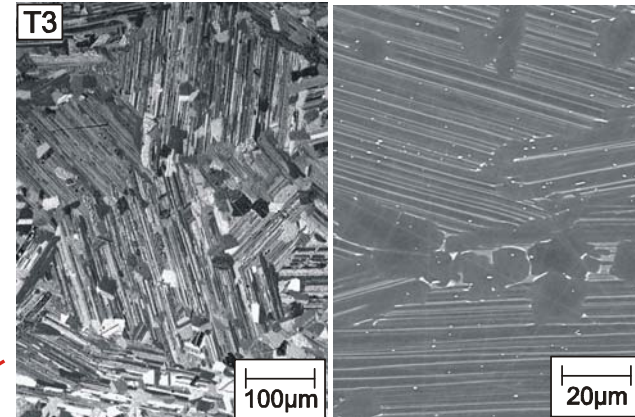
Creep ↑, RT-ductility ↓



Fully Lamellar (FL)

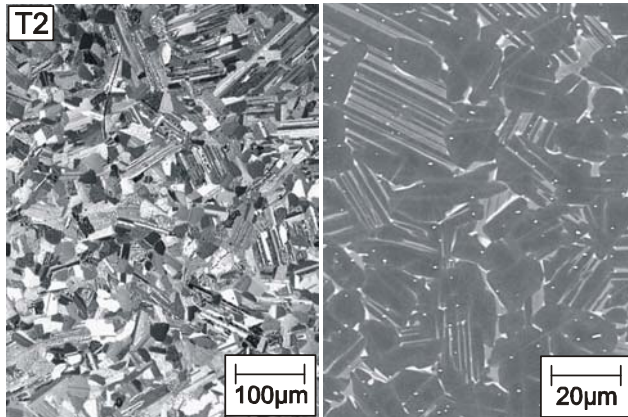


Balanced properties



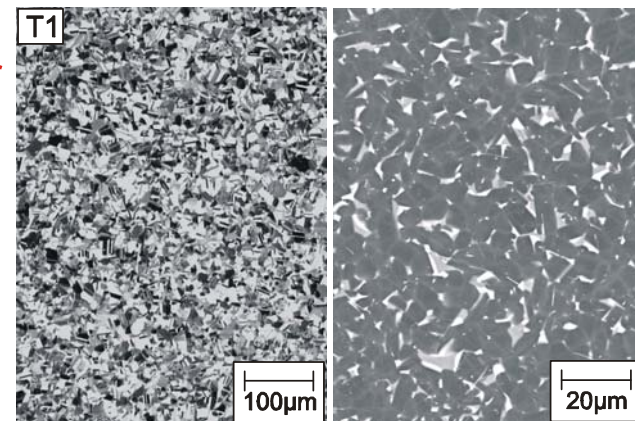
Nearly Lamellar γ (NL γ)

RT-ductility ↑, creep ↓



Duplex (D)

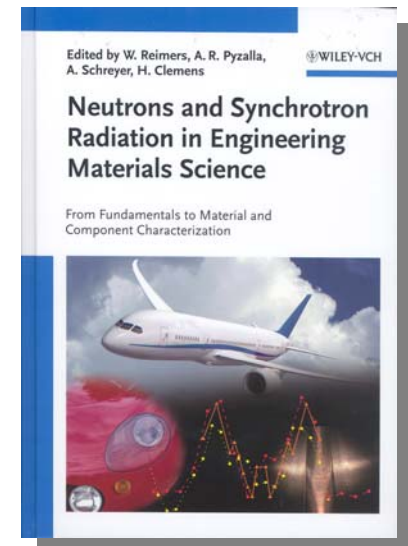
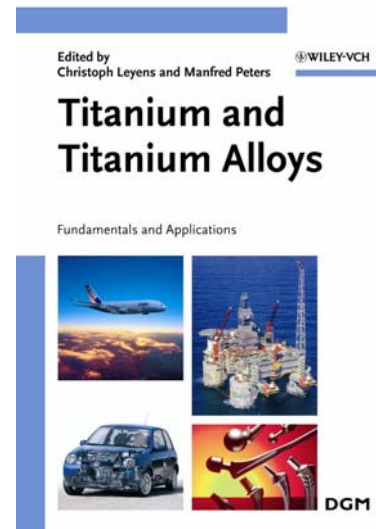
RT-ductility ↑, creep ↓



Near Gamma (NG)

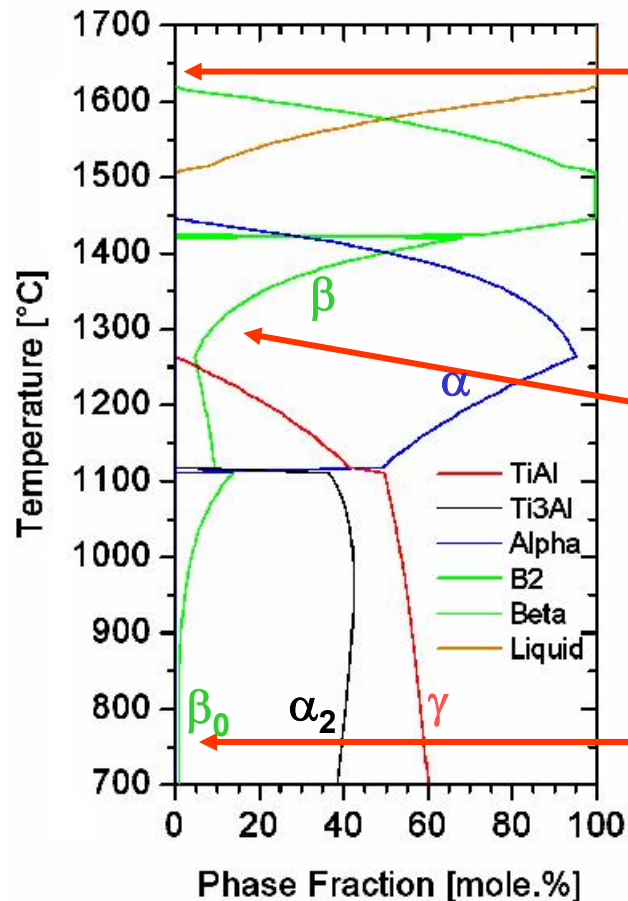


Alloy Development & Alloy Characterization





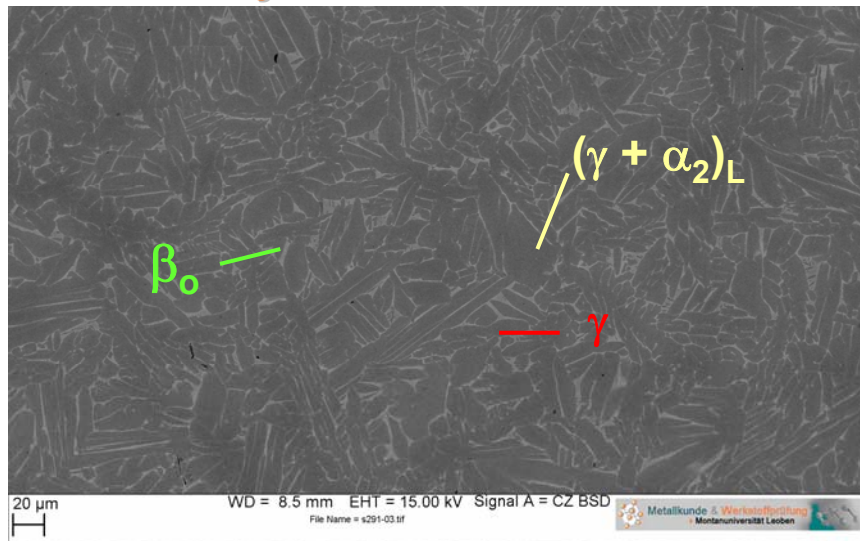
...to aim at good hot-workability and balanced mechanical properties



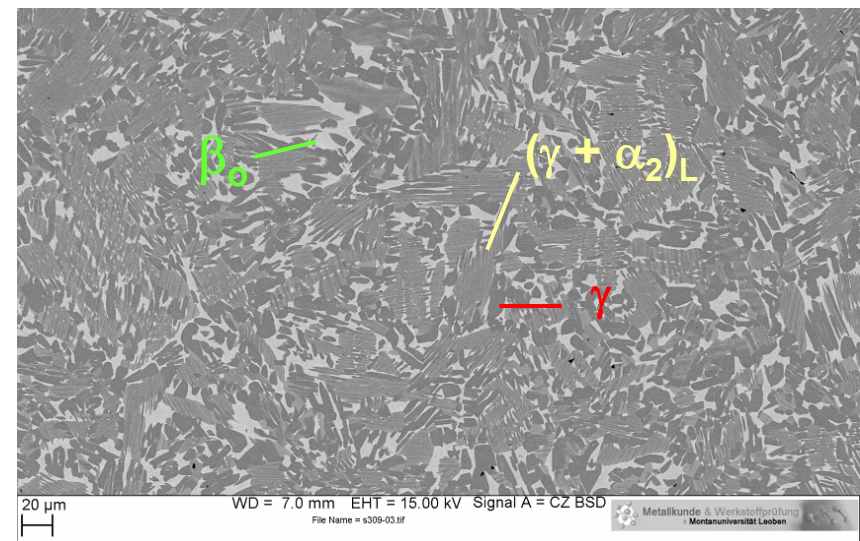
- **Solidification via the β -phase**
- **Minimized segregation and solidification texture**
- **Refined equiaxed microstructure**
→ utilization of borides
- **Presence of ductile bcc β -phase during hot-working**
- **No single α -phase field**
- **Small amount of ordered β_0 -phase at service temperature**
- **Balanced mechanical properties due to optimized micro- and nanostructure**

→ **TNM™ alloys: Ti-(42-45)Al-(3-5)Nb-(0.1-2)Mo-(0.1-1)B**

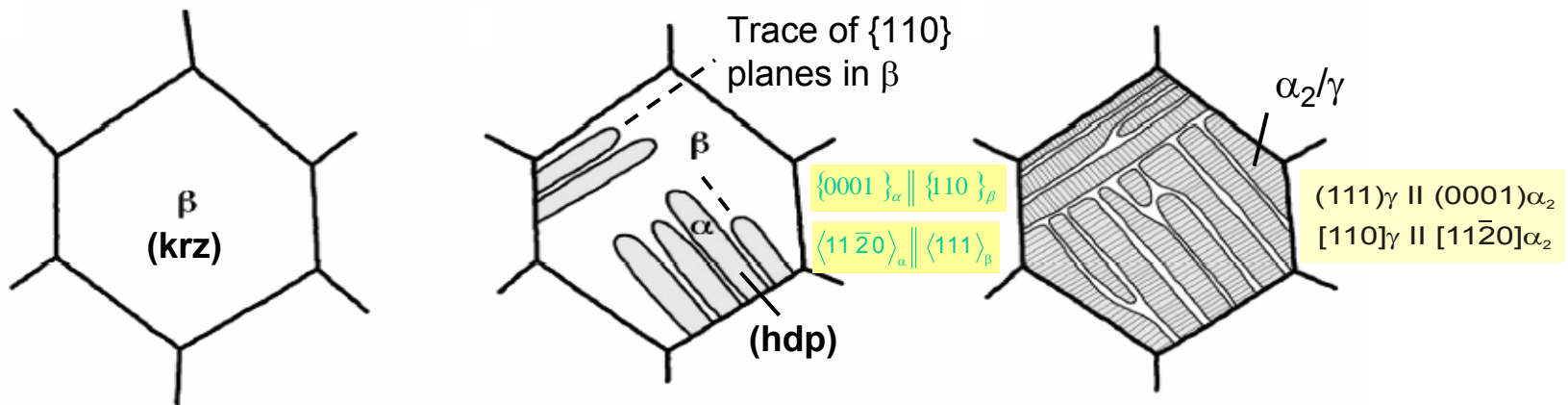
TNM alloy: as-cast microstructure



after HIPing

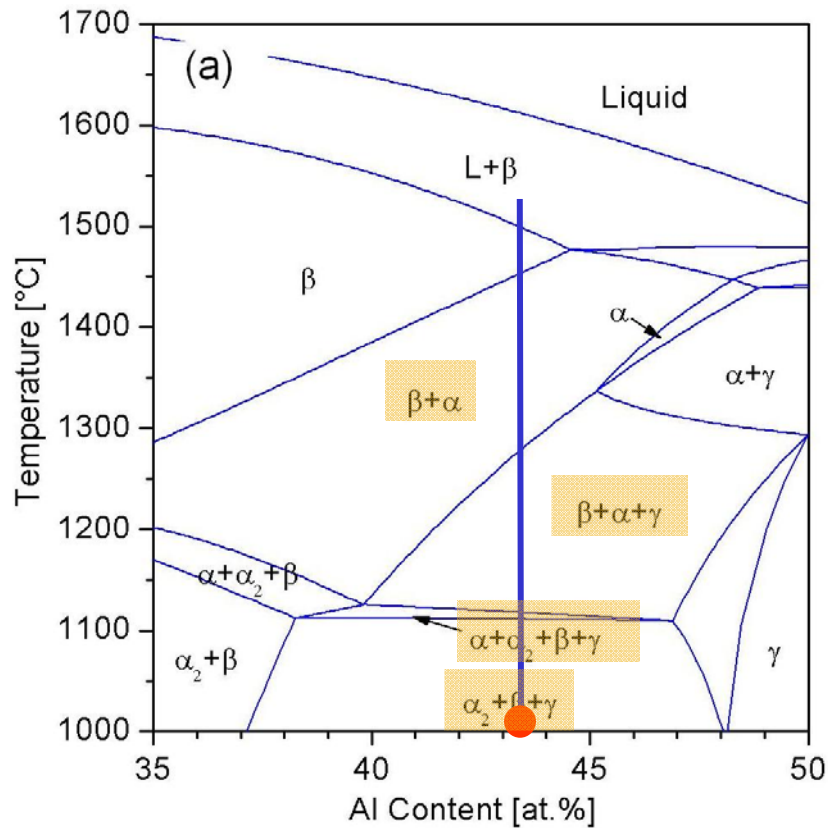


Solidification and transformation model:





Calculated phase diagram

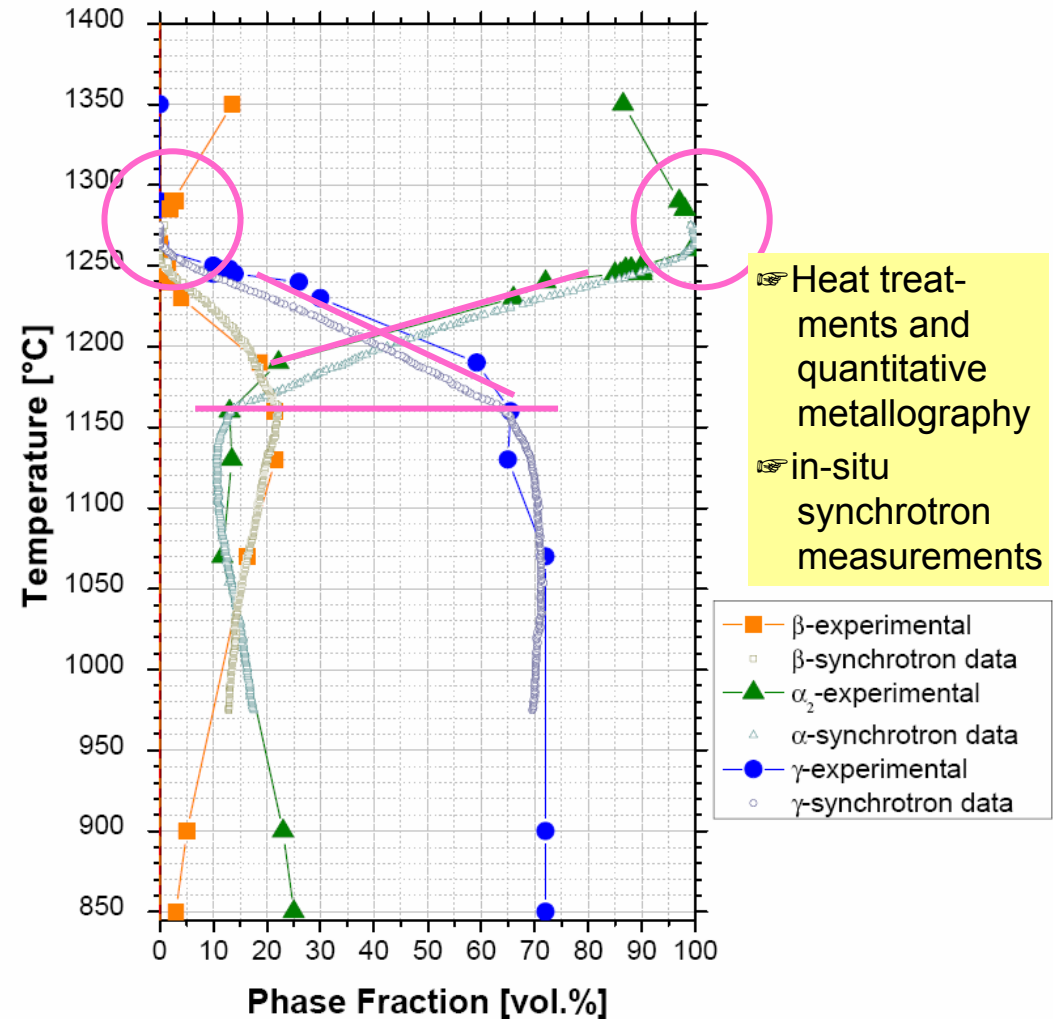
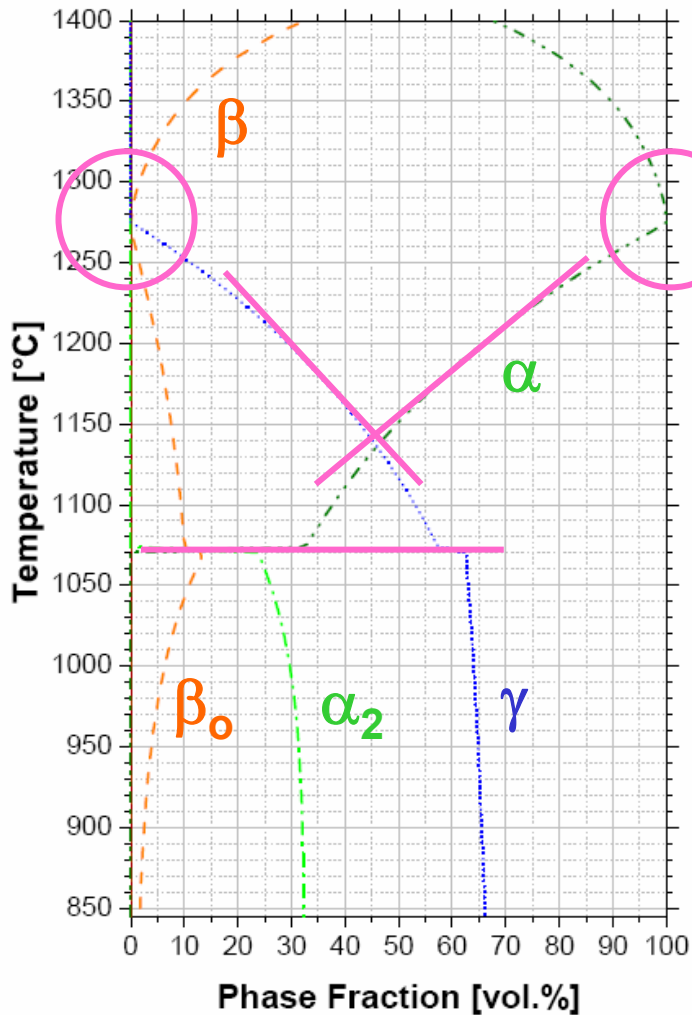


The corresponding diffraction pattern are analyzed by Rietveld method

Calculated

Experimental

Ti-43.9Al-4Nb-0.95Mo-0.1B





Processing



16.12.1991

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Christoph Leyens and Manfred Peters

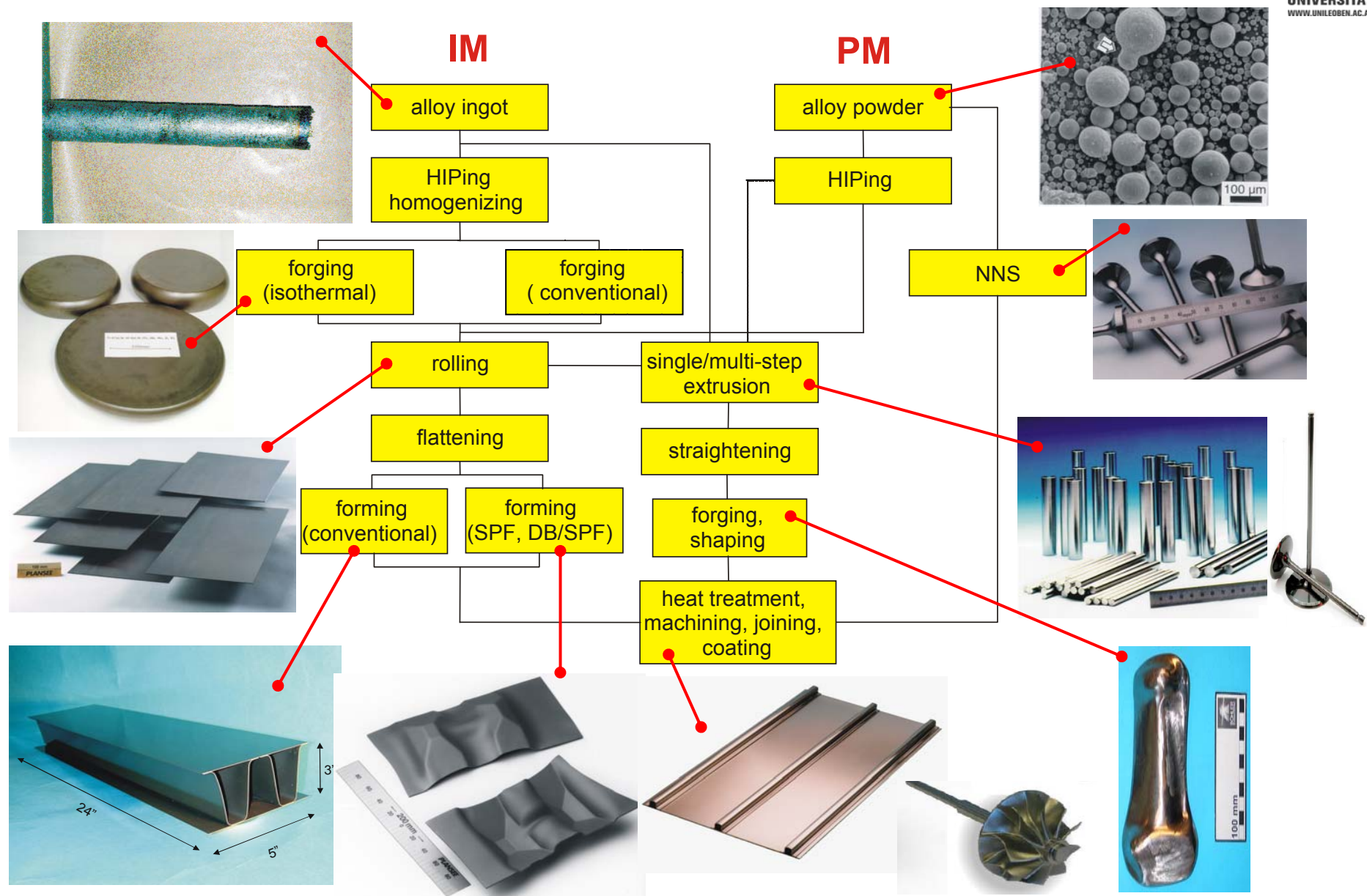
WILEY-VCH

Titanium and Titanium Alloys

Fundamentals and Applications



DGM





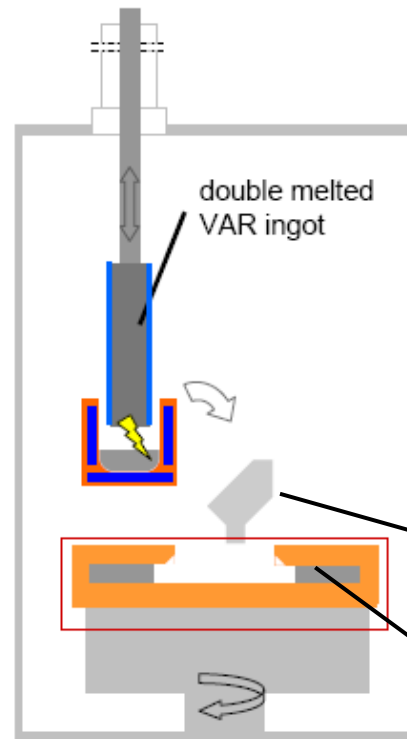
Vacuum Arc Remelting
(VAR)



Large
dimensions

Plasma Arc Melting
(PAM)

VAR skull melter +
centrifugal (spin) casting



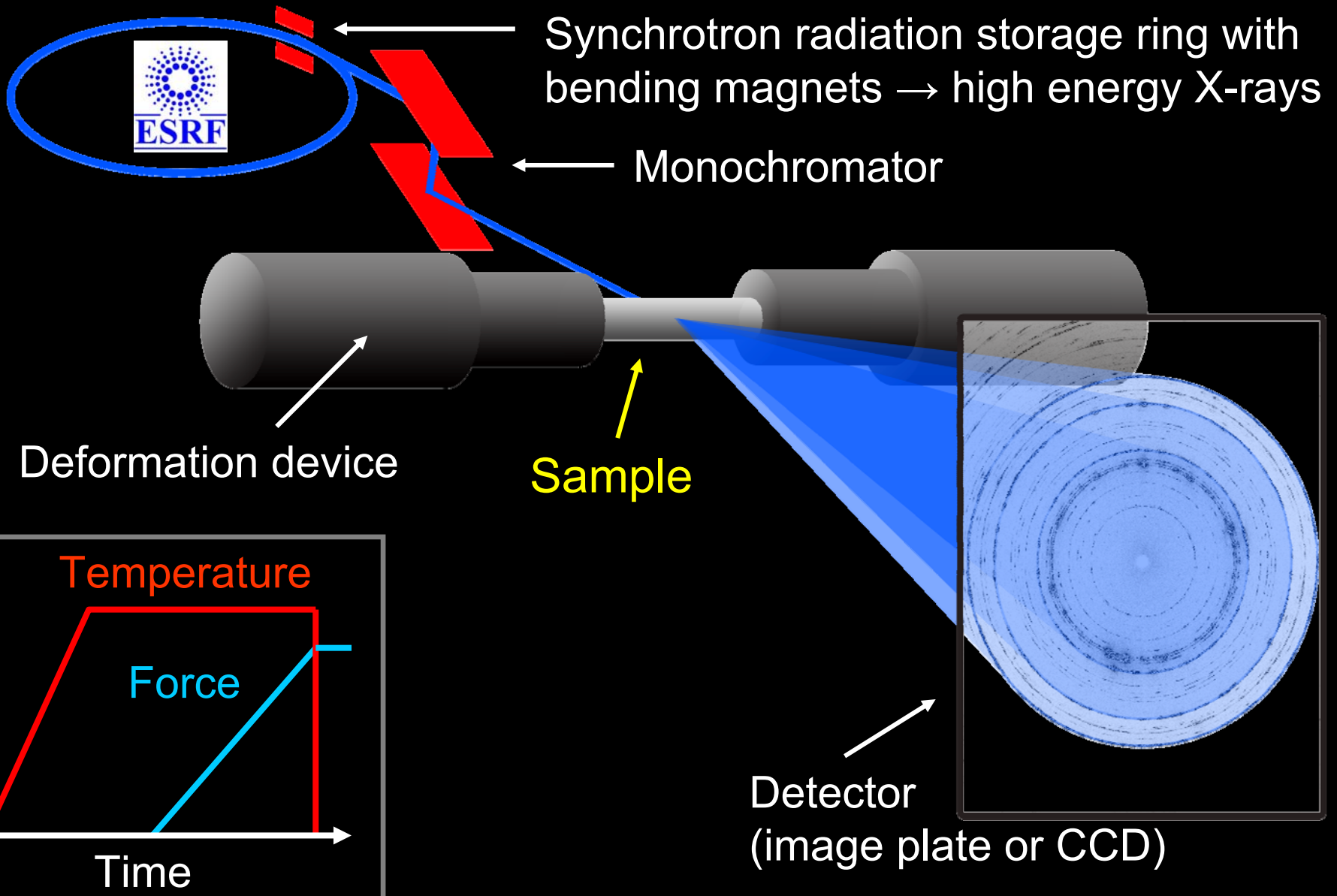
Pouring via **tundish** in
rotating **permanent**
molds

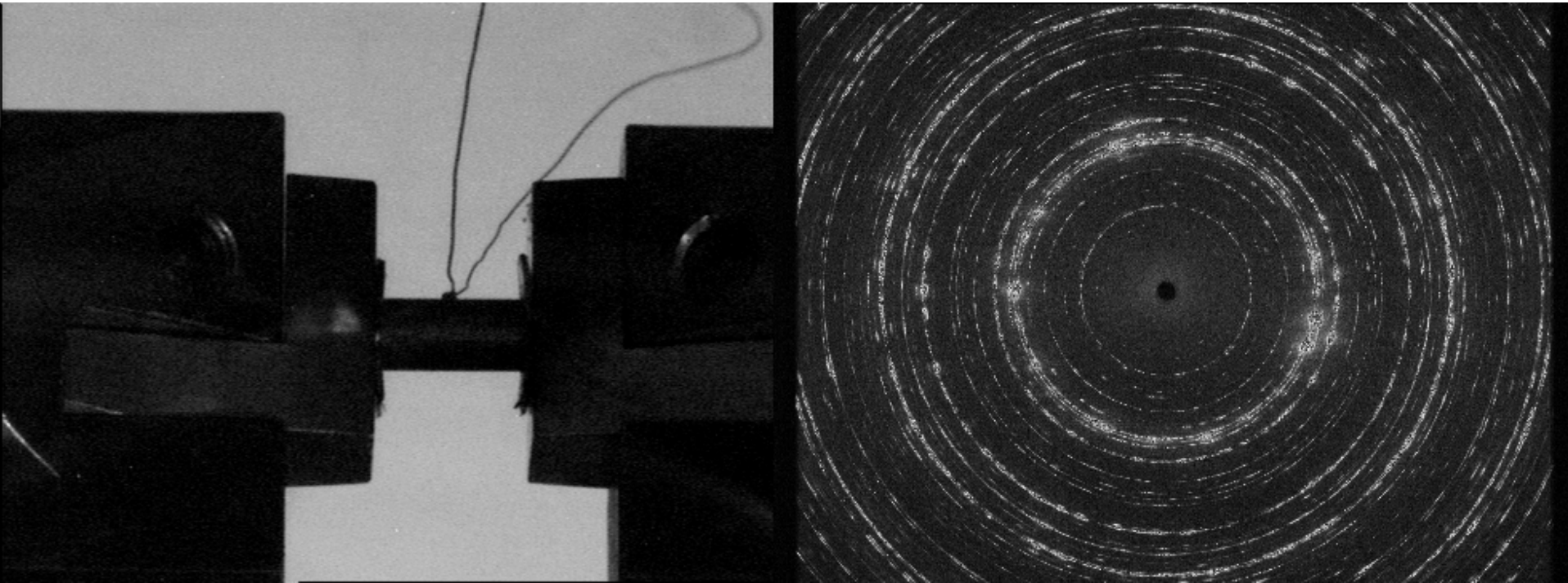


Böhler Schmiedetechnik, Kapfenberg, Austria

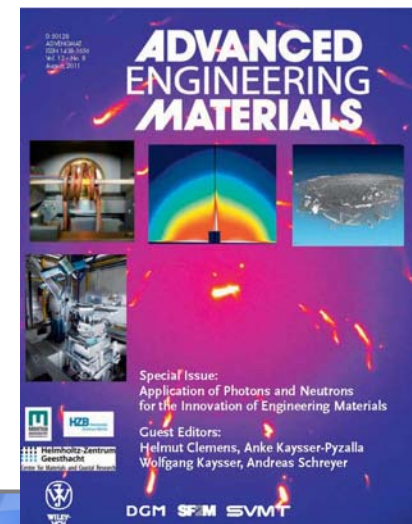
Conventional hot-die forging process







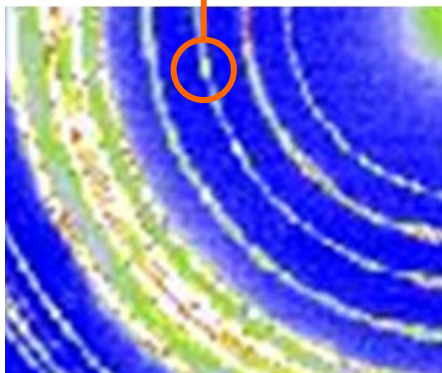
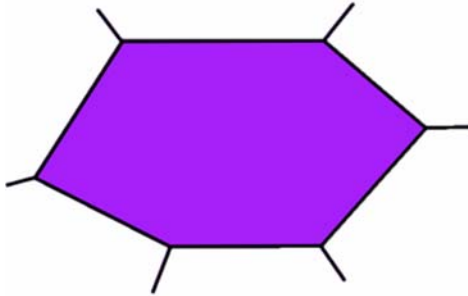
- Information on:**
- phases & phase fractions
 - phase transition temperatures
 - ordering behaviour
 - recrystallization & grain growth behaviour
 - texture



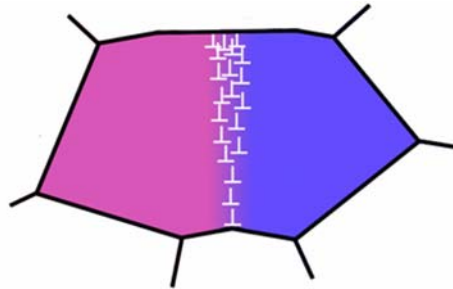


Response of patterns on hot-working, e.g. forging

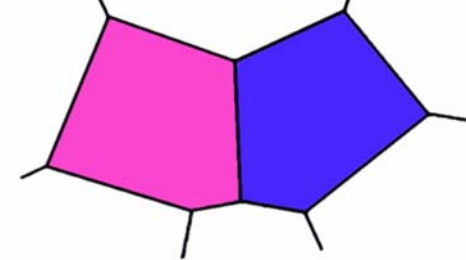
(Perfect) starting
microstructure



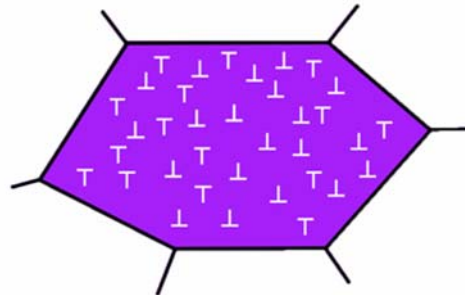
Dynamic recovery



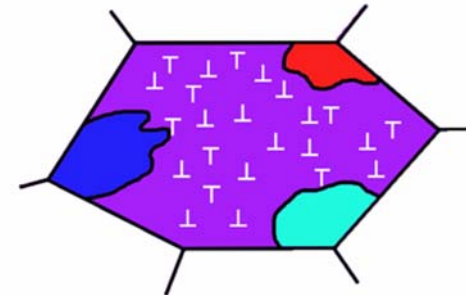
Dynamic (continuous)
recrystallization



(Cold) working



Dynamic recrystallization



deformation & temperature \longrightarrow



- Overall grain refinement occurs during deformation in the $(\alpha+\beta)$ -phase field region
- A high defect density is observed in the α -phase, a lower one in the β -phase

Proposed **predominant processes** occurring during hot-working in the $(\alpha + \beta)$ -phase field region :

- Dislocation slip and slow recovery in α -phase (smaller SFE)
- Slip and very fast recovery in β -phase (higher SFE)
→ extended recovery (in-situ recrystallization)

SFE: stacking fault energy



Microstructure, Heat-Treatments & Mechanical Properties

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Titanium and Titanium Alloys

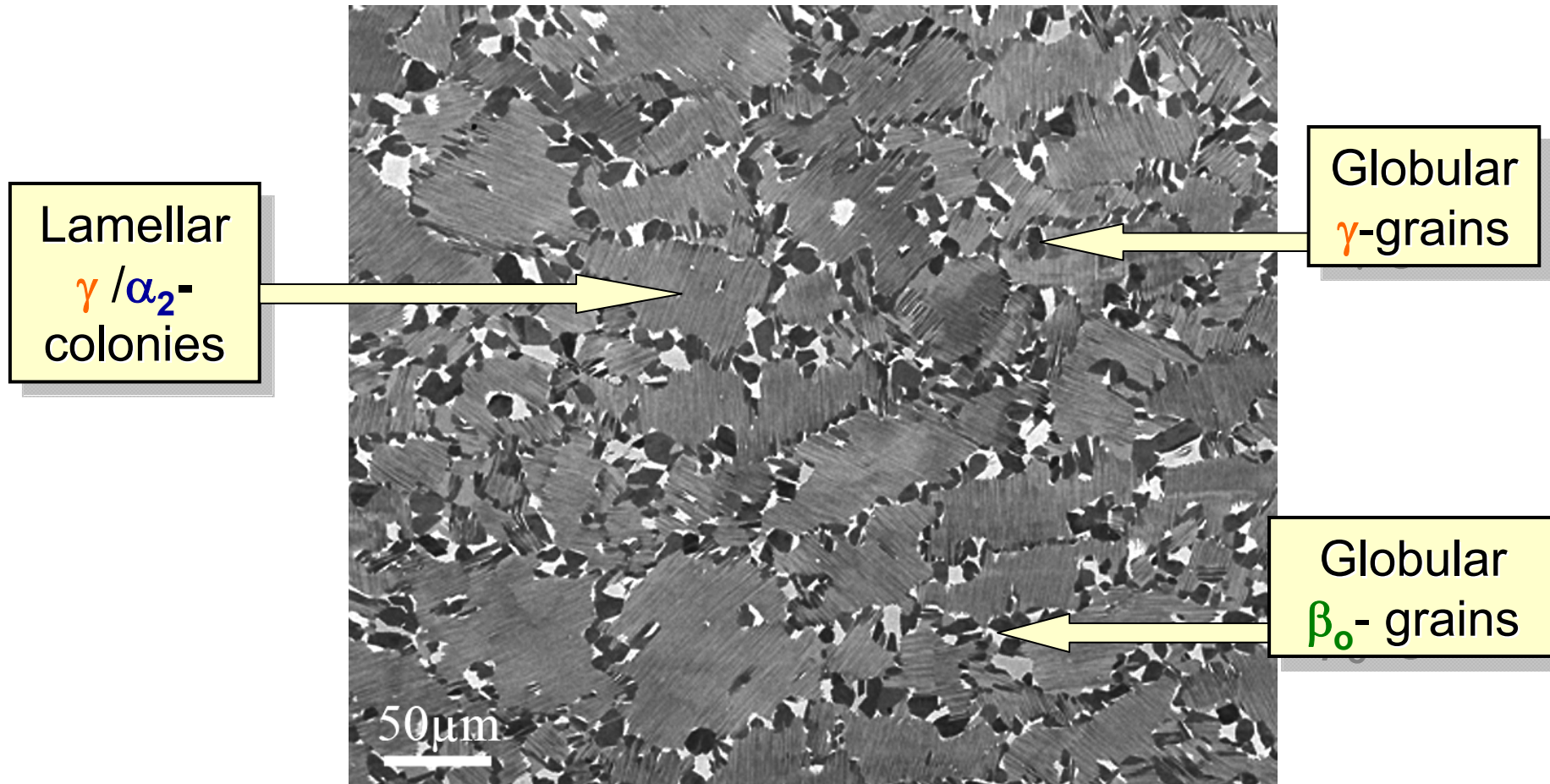
Fundamentals and Applications



DGM



Example of $NL\gamma$ microstructure showing balanced mechanical properties



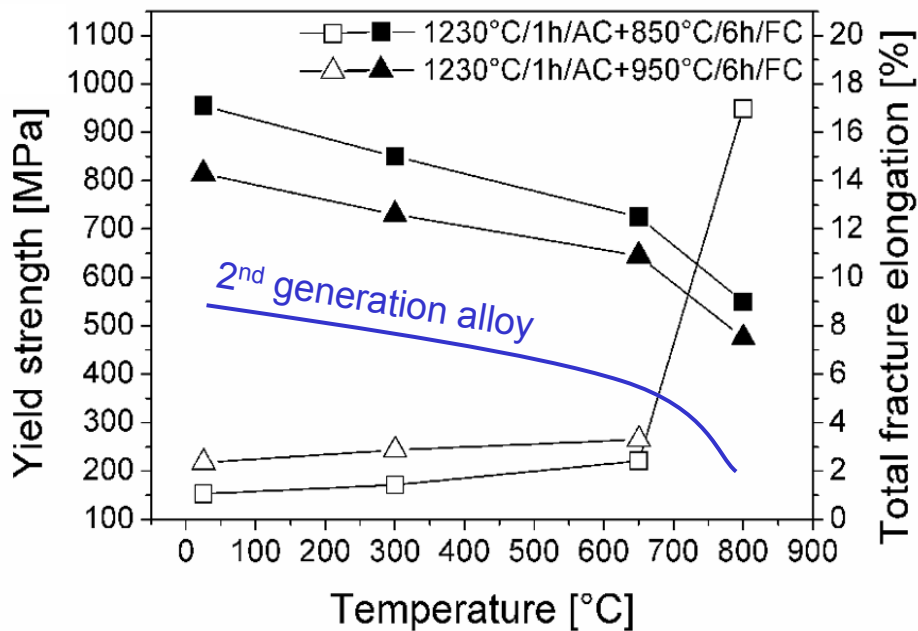
- Microstructural parameters:**
- lamellar colony size and lamellar spacing
 - volume fraction and size of globular β_0 and γ



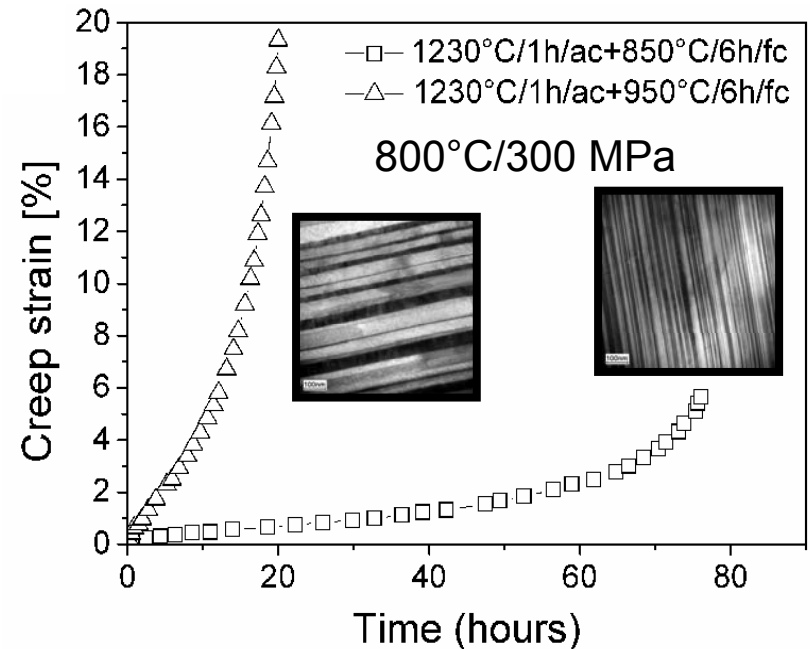
Tensile test

Ti-43at%Al-4at%Nb-1at%Mo-0.1B

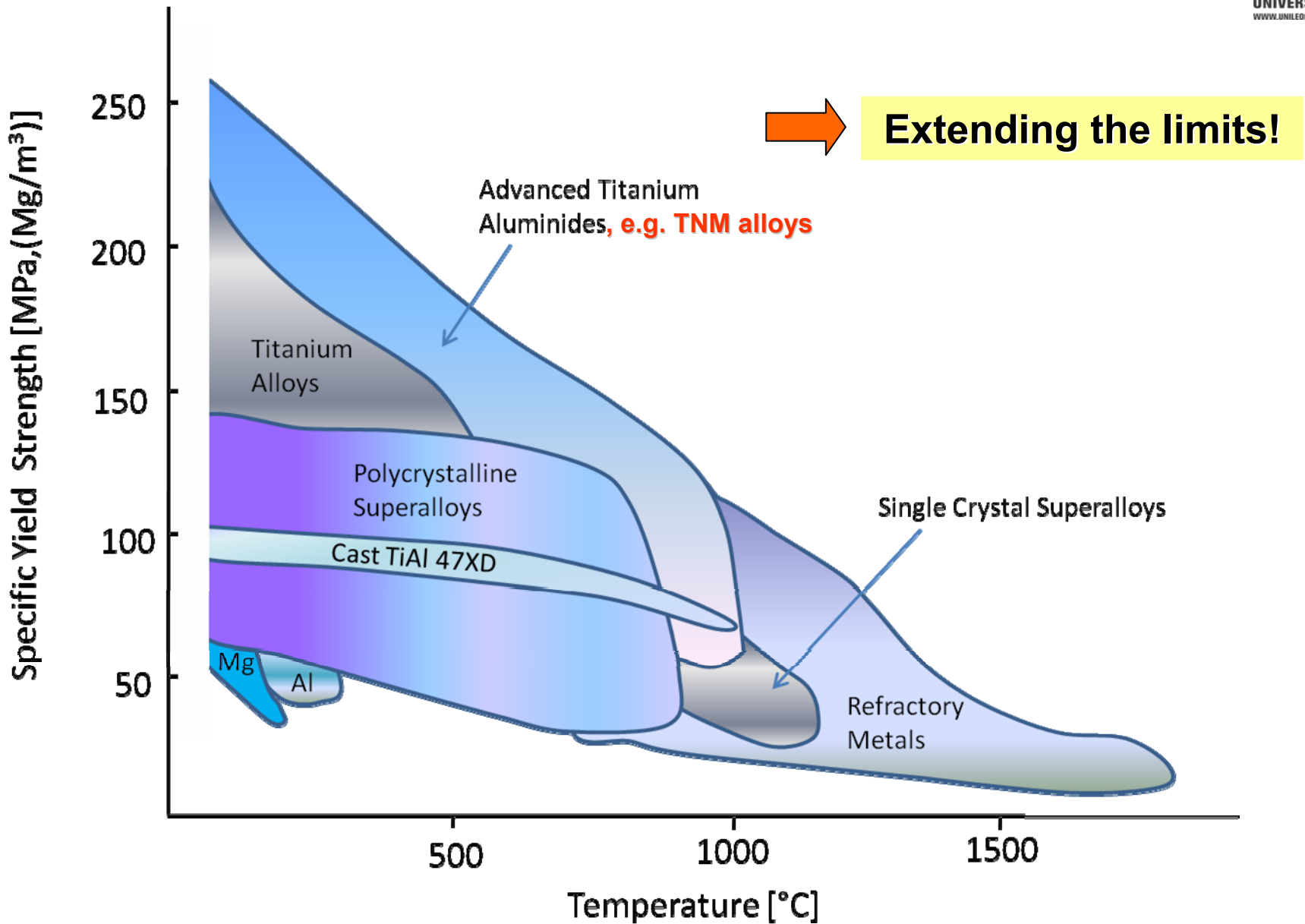
Volume fraction of globular γ - and β_0 -grains is constant!



Creep test



Tensile ductility is mainly determined by the fraction of globular γ -grains!



Wilfried Smarsly, Ulrike Habel, Falko Heutling, Dietmar Helm, *MTU Aero Engines*

Volker Güther, Andreas Otto, Anita Chatterjee, *Matthias Achtermann, GfE*

Daniel Huber, Sascha Kremmer, Martin Stockinger, *Böhler Schmiedetechnik*

Gopal Das, *Pratt & Whitney*

Patrick Voigt, Robert Hempel, *Titanium Solutions*

Masao Takeyama, Hirotoyo Nakashima, *Tokyo Institute of Technology*

Peter Schretter, Heinrich Kestler, *Plansee*

Hartmut Baur, Rainer Joos, *Daimler AG*

Arno Bartels, Wolfram Schillinger, *TU Hamburg Harburg*

Peter Staron, Andreas Stark, Florian Pyczak, Fritz Appel, Michael Oehring, Rainer Gerling, H.-P. Schimansky, *Helmholtz Zentrum Geesthacht*

Klaus-Dieter Liss, Ian Watson, Saurabh Kabra, *ANSTO*

Reinhard Pippan, Otmar Kolednik, Gerhard Dehm, *Erich-Schmid-Institut, Leoben*

Harald Chladil, Dieter Fischer, Limei Cha, Paul Mayrhofer, Ronald Schnitzer, Wolfgang Klauber, Wilfried Wallgram, Barbara Böck, Laura Drössler, Thomas Schmölzer, Martin Schloffer, Emanuel Schwaighofer, Christian Sailer, Lukas Pritz, Eva Eidenberger, Andrea Gaitzenauer, Robert Werner, *Montanuniversität Leoben*

..... and many more !